

TIME - DEPENDENT PERTURBATION THEORY

9.1

→ STUDY OF TIME-DEPENDENT PERTURBATIONS

⇒ TWO-LEVEL SYSTEMS

• H^0 UNPERTURBED HAMILTONIAN

↳ 2 STATES

$$\begin{aligned} |Y_a\rangle & \quad H^0 |Y_a\rangle = E_a |Y_a\rangle \\ |Y_b\rangle & \quad H^0 |Y_b\rangle = E_b |Y_b\rangle \end{aligned}$$

$$\langle Y_a | Y_b \rangle = \delta_{ab}$$

ANY STATE $|\Psi(t=0)\rangle = c_a |Y_a\rangle + c_b |Y_b\rangle$

$$|c_a|^2 + |c_b|^2 = 1$$

$$|\Psi(t)\rangle = c_a e^{-\frac{i}{\hbar} E_a t} |Y_a\rangle + c_b e^{-\frac{i}{\hbar} E_b t} |Y_b\rangle$$

c_a, c_b CONSTANTS

ALL TIME DEPENDENCE
IS IN $e^{-\frac{i}{\hbar} E t}$ FOR
STATIONARY STATES

• TIME-DEPENDENT PERTURBATION

↳ $H'(t)$

$\{ |Y_a\rangle, |Y_b\rangle \}$ FORM A COMPLETE SET



WF AT TIME t CAN STILL BE EXPRESSED AS LINEAR COMBINATION OF $|Y_a\rangle$ & $|Y_b\rangle$

$$|\Psi(t)\rangle = c_a(t) e^{-\frac{i}{\hbar} E_a t} |Y_a\rangle + c_b(t) e^{-\frac{i}{\hbar} E_b t} |Y_b\rangle$$

↑ COEFFICIENTS CAN NOW DEPEND ON TIME ↑

$H'(t)$ CAN INDUCE TRANSITIONS BETWEEN a & b

e.g.	$c_a(t=0) = 1$	$H'(t)$	$c_a(t_1) = 0$
	$c_b(t=0) = 0$	\Rightarrow	$c_b(t_1) = 1$
			$(t_1 > 0)$

↳ $c_a(t), c_b(t)$?

$$H = H^0 + H'(t)$$

$$H |\Psi(t)\rangle = i\hbar \frac{\partial}{\partial t} |\Psi(t)\rangle$$

$$\downarrow \quad |\Psi(t)\rangle = c_a(t) e^{-\frac{i}{\hbar} E_a t} |\mathcal{N}_a\rangle + c_b(t) e^{-\frac{i}{\hbar} E_b t} |\mathcal{N}_b\rangle$$

$$\begin{aligned} & \cancel{c_a e^{-\frac{i}{\hbar} E_a t} H^0 |\mathcal{N}_a\rangle} + \cancel{c_b e^{-\frac{i}{\hbar} E_b t} H^0 |\mathcal{N}_b\rangle} \\ & + c_a e^{-\frac{i}{\hbar} E_a t} H' |\mathcal{N}_a\rangle + c_b e^{-\frac{i}{\hbar} E_b t} H' |\mathcal{N}_b\rangle \\ & = i\hbar \left[\dot{c}_a e^{-\frac{i}{\hbar} E_a t} |\mathcal{N}_a\rangle + \dot{c}_b e^{-\frac{i}{\hbar} E_b t} |\mathcal{N}_b\rangle \right] \\ & + \cancel{c_a E_a e^{-\frac{i}{\hbar} E_a t} |\mathcal{N}_a\rangle} + \cancel{c_b E_b e^{-\frac{i}{\hbar} E_b t} |\mathcal{N}_b\rangle} \end{aligned}$$

$$\begin{aligned} & \Downarrow \\ & c_a e^{-\frac{i}{\hbar} E_a t} H' |\mathcal{N}_a\rangle + c_b e^{-\frac{i}{\hbar} E_b t} H' |\mathcal{N}_b\rangle \\ & = i\hbar \left[\dot{c}_a e^{-\frac{i}{\hbar} E_a t} |\mathcal{N}_a\rangle + \dot{c}_b e^{-\frac{i}{\hbar} E_b t} |\mathcal{N}_b\rangle \right] \end{aligned}$$

$$\begin{aligned} & \Downarrow \quad \langle \mathcal{N}_a | \\ & c_a e^{-\frac{i}{\hbar} E_a t} \langle \mathcal{N}_a | H' | \mathcal{N}_a \rangle + c_b e^{-\frac{i}{\hbar} E_b t} \langle \mathcal{N}_a | H' | \mathcal{N}_b \rangle \\ & = i\hbar \dot{c}_a e^{-\frac{i}{\hbar} E_a t} \end{aligned}$$

DEFINE

$$H'_{ab} \equiv \langle \psi_a | H' | \psi_b \rangle$$

$$H'^{\dagger} = H' \quad (\text{HERMITIAN})$$

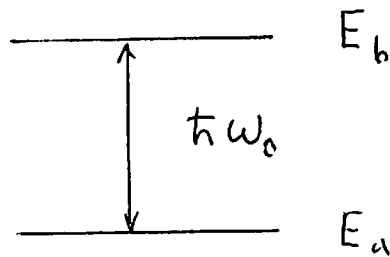
$$H'_{ba} = (H'_{ab})^*$$

$$\dot{c}_a = -\frac{i}{\hbar} \left[c_a H'_{aa} + c_b e^{-\frac{i}{\hbar}(E_b - E_a)t} H'_{ab} \right]$$

ANALOGOUSLY

$$\dot{c}_b = -\frac{i}{\hbar} \left[c_b H'_{bb} + c_a e^{-\frac{i}{\hbar}(E_a - E_b)t} H'_{ba} \right]$$

- IMPORTANT SPECIAL CASE : $H'_{aa} = H'_{bb} = 0$



$$\hbar\omega_0 \equiv E_b - E_a$$

($E_b > E_a$)

$$\dot{c}_a = -\frac{i}{\hbar} c_b e^{-i\omega_0 t} H'_{ab}$$

$$\dot{c}_b = -\frac{i}{\hbar} c_a e^{+i\omega_0 t} H'_{ba}$$

• PERTURBATION THEORY

H' SMALL

↳ SUPPOSE AT $t=0$ SYSTEM IS IN STATE a

$$C_a(t=0) = 1$$

$$C_b(t=0) = 0$$

↳ ZERO ORDER : $H' = 0$

$$C_a^{(0)}(t) = 1$$

$$C_b^{(0)}(t) = 0$$

↳ FIRST ORDER

$$\dot{C}_a^{(1)} = 0 \quad \Rightarrow \quad C_a^{(1)}(t) = 1$$

$$\dot{C}_b^{(1)} = -\frac{i}{\hbar} C_a^{(0)} e^{i\omega_0 t} H'_{ba}(t)$$

↓

$$C_b^{(1)}(t) = -\frac{i}{\hbar} \int_0^t dt' C_a^{(0)}(t') e^{i\omega_0 t'} H'_{ba}(t')$$

$$\approx -\frac{i}{\hbar} \int_0^t dt' e^{i\omega_0 t'} H'_{ba}(t')$$

↳ SECOND ORDER

$$\dot{c}_a^{(2)} = -\frac{i}{\hbar} c_b^{(1)} e^{-i\omega_0 t} H'_{ab}(t)$$

$$c_a^{(2)}(t) - \underbrace{c_a^{(2)}(0)}_1 = -\frac{i}{\hbar} \int_0^t dt' c_b^{(1)}(t') e^{-i\omega_0 t'} H'_{ab}(t')$$

$$c_a^{(2)}(t) = 1 - \frac{1}{\hbar^2} \int_0^t dt' e^{-i\omega_0 t'} H'_{ab}(t') \int_0^{t'} dt'' e^{i\omega_0 t''} H'_{ba}(t'')$$

$$c_b^{(2)}(t) = c_b^{(1)}(t)$$

⋮
ITERATIVE PROCEDURE

↳ NORMALIZATION

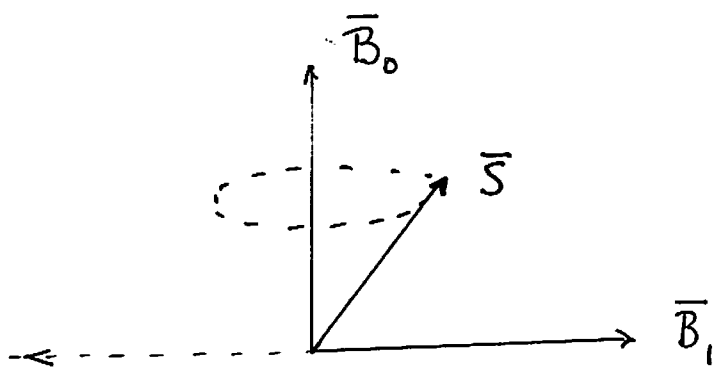
$$|c_a(t)|^2 + |c_b(t)|^2 = 1$$

↑
WILL BE APPROXIMATE
TO THE GIVEN ORDER IN H'

$$\underbrace{|c_a^{(1)}(t)|^2}_1 + \underbrace{|c_b^{(1)}(t)|^2}_{O(H'^2)} = 1 + O(H'^2)$$

• SINUSOIDAL PERTURBATION

↳

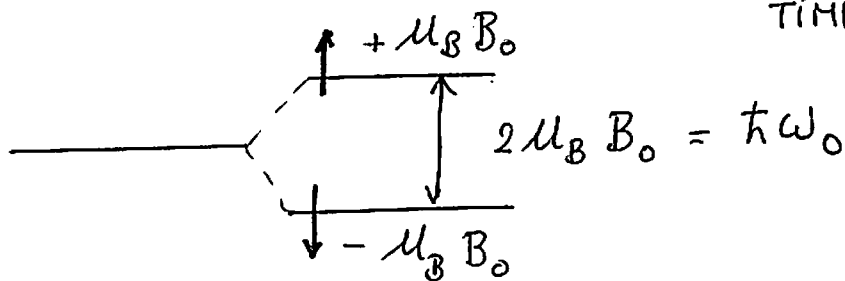


$$\vec{B} = B_0 \hat{e}_z + B_1 \sin \omega t \hat{e}_x$$

$$H^0 = + \frac{e\hbar}{2m} B_0 \sigma_z = \mu_B B_0 \sigma_z$$

$$H^1 = \frac{e\hbar}{2m} B_1 \sin \omega t \sigma_x = \underbrace{\mu_B B_1 \sigma_x}_{\hat{V}} \sin \omega t$$

↑
TIME INDEPENDENT



↳ $H_{ab}^1 = \langle \psi_a | \hat{V} | \psi_b \rangle \sin \omega t$

FOR $\hat{V} = \mu_B B_1 \sigma_x$ $\langle \uparrow | \hat{V} | \uparrow \rangle = 0$

$\langle \downarrow | \hat{V} | \downarrow \rangle = 0$

$V_{\uparrow\downarrow} \equiv \langle \uparrow | \hat{V} | \downarrow \rangle = \langle \downarrow | \hat{V} | \uparrow \rangle = \mu_B B_1$

\hookrightarrow 1^o ORDER

$$|N_a\rangle = |\downarrow\rangle : c_{\downarrow}^{(1)}(t) = 1$$

$$\begin{aligned}
 |N_b\rangle = |\uparrow\rangle : c_{\uparrow}^{(1)}(t) &= -\frac{i}{\hbar} \int_0^t dt' e^{i\omega_0 t'} V_{ba} \sin \omega t' \\
 &= -\frac{i V_{ba}}{\hbar} \frac{1}{2i} \int_0^t dt' \left[e^{i(\omega_0 + \omega)t'} - e^{i(\omega_0 - \omega)t'} \right] \\
 &= -\frac{V_{ba}}{2\hbar} \left\{ \frac{e^{i(\omega_0 + \omega)t} - 1}{i(\omega_0 + \omega)} - \frac{e^{i(\omega_0 - \omega)t} - 1}{i(\omega_0 - \omega)} \right\}
 \end{aligned}$$

\Downarrow

FOR DRIVING FREQUENCIES

$$\omega \approx \omega_0$$

↑
CLOSE TO TRANSITION FREQ. ω_0

$$\omega_0 + \omega \gg |\omega_0 - \omega|$$

$$\begin{aligned}
 c_{\uparrow}^{(1)}(t) &= +\frac{V_{\uparrow\downarrow}}{2i\hbar} \frac{e^{i(\omega_0 - \omega)t} - 1}{(\omega_0 - \omega)} \\
 &= \frac{V_{\uparrow\downarrow}}{2i\hbar} \frac{e^{i(\omega_0 - \omega)t/2}}{\omega_0 - \omega} \left[e^{i(\omega_0 - \omega)t/2} - e^{-i(\omega_0 - \omega)t/2} \right]
 \end{aligned}$$

$$c_{\uparrow}^{(1)}(t) = \frac{V_{\uparrow\downarrow}}{\hbar} \frac{\sin[(\omega_0 - \omega)t/2]}{(\omega_0 - \omega)} e^{i(\omega_0 - \omega)t/2} \quad 9.9$$

↳ TRANSITION PROBABILITY $\downarrow \rightarrow \uparrow$ (SPIN FLIP)

$$P_{\downarrow \rightarrow \uparrow}(t) = |c_{\uparrow}^{(1)}(t)|^2$$

$$\approx \frac{|V_{\uparrow\downarrow}|^2}{\hbar^2} \frac{\sin^2[(\omega_0 - \omega)t/2]}{(\omega_0 - \omega)^2}$$

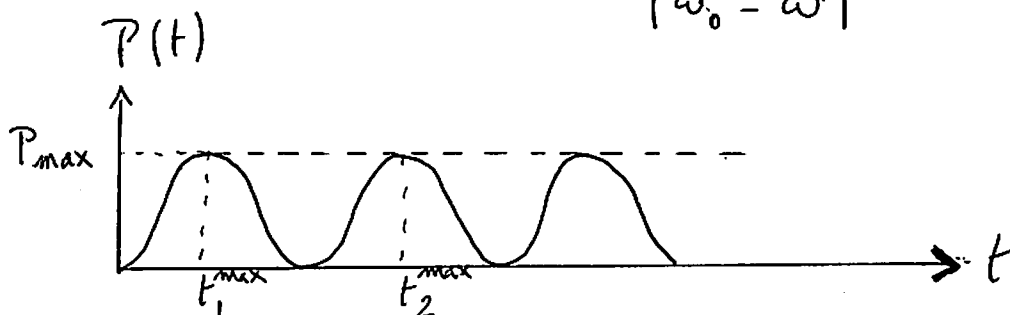
PROBABILITY OF SPIN FLIP AT TIME t

$$P_{\downarrow \rightarrow \uparrow}(0) = 0$$

$$P_{\downarrow \rightarrow \uparrow} \text{ RISES TO MAX. } \frac{|V_{\uparrow\downarrow}|^2}{\hbar^2 (\omega_0 - \omega)^2} = \frac{(\mu_B B_1)^2}{\hbar^2 (\omega_0 - \omega)^2}$$

$$\hbar \omega_0 = 2\mu_B B_0$$

$$\text{AT TIMES } t_m^{\text{max}} = \frac{(2m+1)\pi}{|\omega_0 - \omega|}$$



↳ AT A TIME t

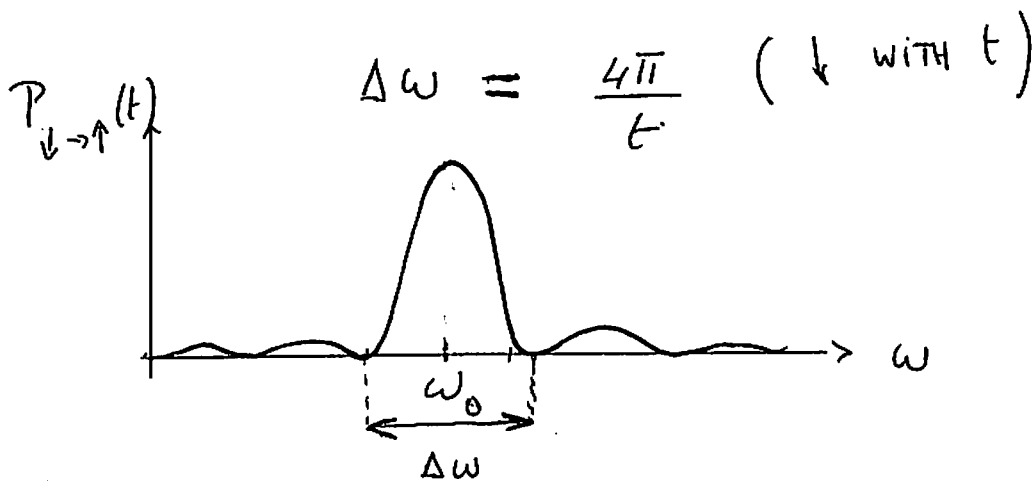
VARY ω

FOR $\omega \approx \omega_0$

$$\sin^2 \left[(\omega_0 - \omega) t/2 \right] \approx (\omega_0 - \omega)^2 \frac{t^2}{4}$$

$$P_{\downarrow \rightarrow \uparrow}(t) \approx \left(\frac{|V_{\uparrow \downarrow}| t}{2\hbar} \right)^2 \quad \text{HEIGHT (}\uparrow\text{ WITH }t\text{)}$$

$$\text{WIDTH } \frac{\Delta\omega t}{2} = (2\pi)$$



RESONANCE WHEN $\omega \rightarrow \omega_0$

CAVEAT

: IF $P_{\downarrow \rightarrow \uparrow}(t) \uparrow$ AT SOME POINT P.T.
BREAKS DOWN

EXACT SOLUTION $P_{\downarrow \rightarrow \uparrow}(t) \leq 1$ EVIDENTLY!

• EXACT SOLUTION : ROTATING WAVE METHOD

$$\begin{aligned} \hookrightarrow H' &= \hat{V} \sin \omega t \\ &= \hat{V} \frac{1}{2i} (e^{i\omega t} - e^{-i\omega t}) \end{aligned}$$

↳ RABI'S METHOD

$$C_b(t) = -\frac{V_{ba}}{2\hbar} \left\{ \frac{e^{i(\omega_0 + \omega)t} - 1}{i(\omega_0 + \omega)} - \frac{e^{i(\omega_0 - \omega)t} - 1}{i(\omega_0 - \omega)} \right\}$$

\uparrow $i\omega t$ FROM e PART IN H' \uparrow $-i\omega t$ FROM e PART IN H'

FOR $\omega \approx \omega_0$ KEEP ONLY 2^0 TERM

$$H' = \hat{V} \left(\frac{i}{2} \right) e^{-i\omega t}$$

ROTATING WAVE

↳ WITH THIS H' , WE CAN SOLVE PROBLEM EXACTLY, WITHOUT USING PT

$$\begin{aligned} H'_{aa} &= H'_{bb} = 0 \\ H'_{ba} &= V_{ba} \frac{i}{2} e^{-i\omega t} \\ H'_{ab} &= H'_{ba}^* = V_{ab}^* \left(-\frac{i}{2} \right) e^{+i\omega t} \end{aligned}$$

↳ GENERAL SOLUTION FOR $H' = \hat{V} \left(\frac{i}{2}\right) e^{-i\omega t}$ 9.12

$$\begin{cases} \dot{c}_a = -\frac{i}{\hbar} c_b e^{-i\omega_0 t} & H'_{ab} \\ \dot{c}_b = -\frac{i}{\hbar} c_a e^{+i\omega_0 t} & H'_{ba} \end{cases}$$

⇓

$$\begin{cases} \dot{c}_a = -\frac{1}{2\hbar} V_{ab}^* e^{i(\omega - \omega_0)t} c_b \\ \dot{c}_b = +\frac{1}{2\hbar} V_{ba} e^{-i(\omega - \omega_0)t} c_a \end{cases}$$

$$\begin{aligned} \ddot{c}_b &= \frac{1}{2\hbar} V_{ba} e^{-i(\omega - \omega_0)t} \left[-i(\omega - \omega_0) c_a + \dot{c}_a \right] \\ &= -i(\omega - \omega_0) \dot{c}_b - \frac{1}{(2\hbar)^2} |V_{ab}|^2 c_b \end{aligned}$$

$$\ddot{c}_b + i(\omega - \omega_0) \dot{c}_b + \frac{1}{(2\hbar)^2} |V_{ab}|^2 c_b = 0$$

TRY $c_b \sim e^{i\lambda t}$

$$-\lambda^2 - i(\omega - \omega_0)\lambda + \frac{1}{(2\hbar)^2} |V_{ab}|^2 = 0$$

$$\lambda^2 + (\omega - \omega_0) \lambda - \frac{1}{(2\hbar)^2} |V_{ab}|^2 = 0$$

$$\lambda = -\frac{(\omega - \omega_0)}{2} \pm \frac{1}{2} \sqrt{(\omega - \omega_0)^2 + \frac{|V_{ab}|^2}{\hbar^2}}$$

$$\omega_R \equiv \frac{1}{2} \sqrt{(\omega - \omega_0)^2 + \frac{|V_{ab}|^2}{\hbar^2}}$$

↑
RABI FLOPPING FREQUENCY

$$\begin{aligned} \therefore c_b(t) &= A e^{i \left[-\frac{(\omega - \omega_0)}{2} + \omega_R \right] t} \\ &+ B e^{i \left[-\frac{(\omega - \omega_0)}{2} - \omega_R \right] t} \\ &= e^{-i \frac{(\omega - \omega_0)}{2} t} \left[A e^{i \omega_R t} + B e^{-i \omega_R t} \right] \end{aligned}$$

OR EQUIVALENTLY

$$c_b(t) = e^{-i \frac{(\omega - \omega_0)}{2} t} \left[C \cos \omega_R t + D \sin \omega_R t \right]$$

$$\leadsto c_b(t=0) = 0 \Rightarrow C = 0$$

$$\| c_b(t) = D e^{-i \frac{(\omega - \omega_0)}{2} t} \sin \omega_R t$$

$$\begin{aligned} \rightsquigarrow c_a(t) &= \frac{2\hbar}{V_{ba}} \dot{c}_b e^{+i(\omega - \omega_0)t} \\ &= \frac{2\hbar}{V_{ba}} D \left[-\frac{i(\omega - \omega_0)}{2} \sin \omega_R t + \omega_R \cos \omega_R t \right] e^{i\frac{(\omega - \omega_0)t}{2}} \end{aligned}$$

$$c_a(t=0) = 1 \quad \Rightarrow \quad \frac{2\hbar}{V_{ba}} D \omega_R = 1$$

$$D = \frac{V_{ba}}{2\hbar\omega_R}$$

$$\begin{aligned} \rightsquigarrow c_a(t) &= e^{i\frac{(\omega - \omega_0)t}{2}} \left[\cos \omega_R t - i \frac{(\omega - \omega_0)}{2\omega_R} \sin \omega_R t \right] \\ c_b(t) &= \frac{V_{ba}}{2\hbar\omega_R} e^{-i\frac{(\omega - \omega_0)t}{2}} \sin \omega_R t \end{aligned}$$

THESE EXPRESSIONS ARE EXACT FOR $\omega \approx \omega_0$
 IN CONTRAST TO P.T. RESULTS

CHECK : $|c_a(t)|^2 + |c_b(t)|^2 = 1$ (EXACT!)

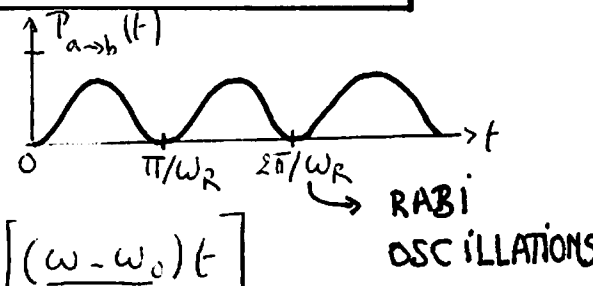
↳ PROBABILITY FOR TRANSITION $a \rightarrow b$

$$P_{a \rightarrow b}(t) = |c_b(t)|^2 = \frac{|V_{ba}|^2}{(2\hbar\omega_R)^2} \sin^2 \omega_R t$$

↳ EXACT RESULT $\omega \approx \omega_0$

↳ COMPARE WITH P.T. RESULT

$$P_{a \rightarrow b}^{PT}(t) = \frac{|V_{ba}|^2}{(\hbar(\omega - \omega_0))^2} \sin^2 \left[\frac{(\omega - \omega_0)t}{2} \right]$$



PT RESULT IS OBTAINED FOR

$$|V_{ab}| \ll \hbar(\omega - \omega_0)$$

↓

$$\omega_R = \frac{1}{2}(\omega - \omega_0)$$

↳ PT DOES NOT HOLD VERY CLOSE TO RESONANCE ($\omega = \omega_0$)

↳ EXACT RESULT

MAX. FOR $\omega_R t = (2m+1) \frac{\pi}{2}$

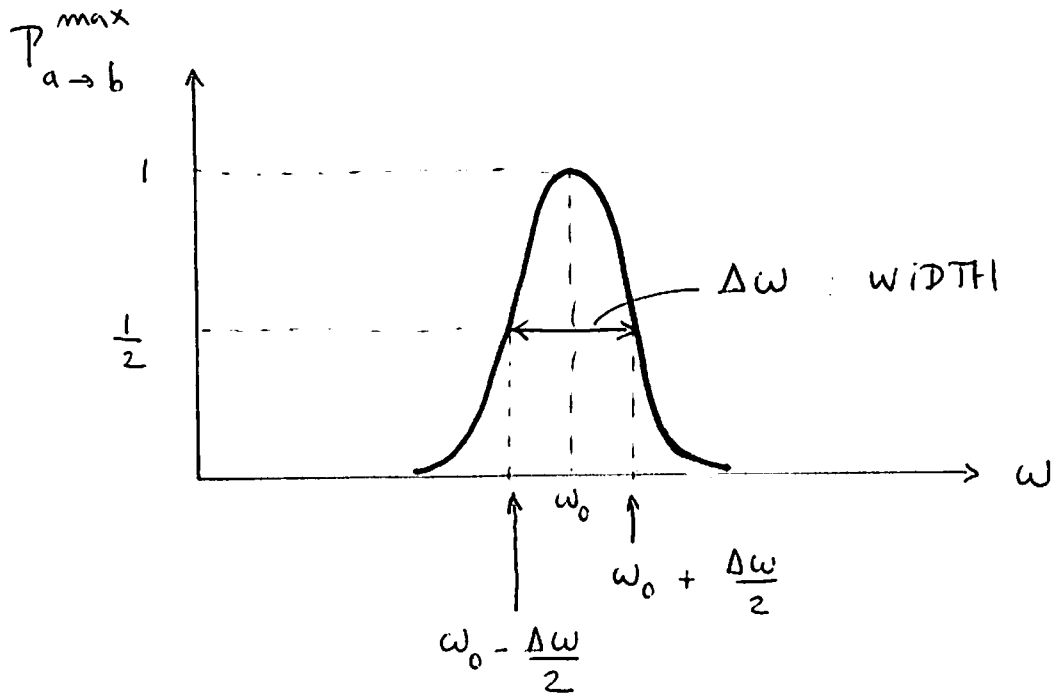
$$t = \frac{(2m+1)\pi}{2\omega_R}$$

MAX PROBABILITY $P_{a \rightarrow b}^{max} = \frac{|V_{ba}|^2}{(2\hbar\omega_R)^2}$

WHEN $\omega = \omega_0 \Rightarrow \omega_R = \frac{|V_{ab}|}{2\hbar} \Rightarrow P_{a \rightarrow b}^{max} = 1$

$$P_{a \rightarrow b}^{\max} = \frac{|V_{ba}|^2 / \hbar^2}{(\omega - \omega_0)^2 + |V_{ba}|^2 / \hbar^2}$$

↓
RESONANCE FOR $\omega = \omega_0$

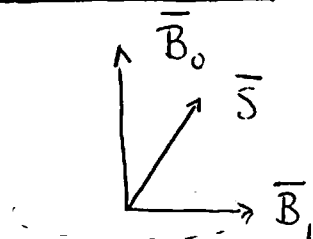


$$\frac{\Delta\omega}{2} = \frac{|V_{ba}|}{\hbar}$$

$\Delta\omega$ ALSO CALLED
FULL WIDTH AT HALF MAXIMUM

FOR $\omega = \omega_0 \pm \frac{\Delta\omega}{2} \Rightarrow P_{a \rightarrow b}^{\max} = \frac{1}{2}$

• APPLICATION : NUCLEAR MAGNETIC RESONANCE (NMR)



$$\omega_0 = \frac{e}{2M_p} g_p B_0$$

↑ ||
PROTON MASS 5.59

FOR $B_0 = 1T \Rightarrow \frac{\omega_0}{2\pi} = 4.3 \cdot 10^7 \text{ Hz}$

RESONANCE FREQUENCY OBTAINED FOR RF (RADIO FREQ.) B_1 FIELD